APPENDIX C

COMPUTATION PROCEDURE FOR EXTREME VALUE (GUMBEL) DISTRIBUTION

(Reproduced from reference 48.)

5.2.6.1.2 Computational methods

It can be shown that most frequency functions applicable to hydrological analysis can take the form

$$X_{T_r} = \overline{X} + Ks_x \tag{5.1}$$

where \overline{X} is the mean value, and s_x is the standard deviation of the variable being studied. Value X_{T_r} denotes the magnitude of the event reached or exceeded on an average once in T_r years. K is the frequency factor. If X is not normally distributed, K depends on frequency and skewness coefficient. A commonly used distribution of extreme values (annual series) is the double exponential distribution, which has been widely applied by Gumbel (see Bibliography), and often bears his name. In this method

$$K = \frac{Y_{T_r} - \overline{Y}_n}{s_n} \tag{5.2}$$

where \overline{Y}_n , the reduced mean, and s_n , the reduced standard deviation, are functions only of sample size; and Y_{T_n} , the reduced variate, is related to return period by

$$Y_{T_r} = -\left(0.83405 + 2.30259 \log \log \frac{T_r}{T_r - 1}\right)$$
 (5.3)

Table 5.3 gives values of K computed by means of Eq. (5.2) using Gumbel's values for \overline{Y}_n , s_n , and Y_{T_p} .

There are two basic methods for fitting data to the extreme value distribution. One consists in computation of X_{T_r} by means of Eq. (5.1), after a previous computation of the values of \overline{X} and s_x (Table 5.4). The other consists in plotting data on suitable graph paper, known as extreme probability paper, and drawing a line by inspection.

TABLE 5.3

Values of K based on Eq. (5.2)

	Return period (years)								
n	2	5	10	25	50	100			
10	0.1355	1.0580	1.8483	2.8467	3.5874	4.3227			
11	 0. 137 6	1.0338	1.8094	2.7894	3.5163	4.2379			
12	0.1393	1.0134	1.7766	2.7409	3.4563	4.1664			
13	-0.1408	.9958	1.7484	2.6993	3.4048	4.1050			
14	-0.1422	.9806	1.7240	2.6632	3.3600	4.0517			
15	0.1434	.9672	1.7025	2.6316	3.3208	4.0049			
16	-0.1444	.9553	1.6835	2.6035	3.2860	3.9635			
17	-0.1454	.9447	1.6665	2.5784	3.2549	3.9265			
18	0.1463	.9352	1.6512	2.5559	3.2270	3.8932			
19	0.1470	.9265	1.6373	2.5354	3.2017	3.8631			
20	-0.1478	.9187	1.6247	2.5169	3.1787	3.8356			
21	-0.1484	.9115	1.6132	2.4999	3.1576	3.8106			
22	0.1490	.9049	1.6026	2.4843	3.1383	3.7875			
23	0.1496	.8988	1.5929	2.4699	3.1205	3.7663			
24	— 0. 1501	.8931	1.5838	2.4565	3.1040	3.7466			
25	-0.1506	.8879	1.5754	2.4442	3.0886	3.7283			
26	-0.1510	.8830	1.5676	2.4326	3.0743	3.7113			
27	— 0. 1515	.8784	1.5603	2.4219	3.0610	3.6954			
28	0.1518	.8742	1.5535	2.4118	3.0485	3.6805			
29	0.1522	.8701	1.5470	2.4023	3.0368	3.6665			

(continued)

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TABLE 5.3 (continued)

Return period (years)

	neturn period (years)								
n	2	5	10	25	50	100			
30	0.1526	.8664	1.5410	2.3934	3.0257	3.6534			
31	-0.1529	.8628	1.5353	2.3850	3.0153	3.6410			
32	-0.1532	.8594	1.5299	2.3770	3.0054	3.6292			
33	 0. 153 5	.8562	1.5248	2.3695	2.9961	3.618 1			
34	-0.1538	.8532	1.5199	2.3623	2.9873	3.6076			
35	0.1540	.8504	1.5153	2.3556	2.9789	3.5976			
36	-0.1543	.8476	1.5110	2.3491	2.9709	3.5881			
37	0.1545	.8450	1.5068	2.3430	2.9633	3.5790			
38	0.1548	.8425	1.5028	2.3371	2.9561	3.5704			
39	-0.1550	.8402	1.4990	2.3315	2.9491	3.5622			
40	-0.1552	.8379	1.4954	2.3262	2.9425	3.5543			
41	-0.1554	.8357	1.4920	2.3211	2.9362	3.5467			
42	0.1556	.8337	1.4886	2.3162	2.9301	3.5395			
43	 0. 1557	.8317	1.4854	2.3115	2.9243	3.5325			
44	0.1559	.8298	1.4824	2.3069	2.9187	3.5259			
45	0.1561	.827 9	1.4794	2.3026	2.9133	3.5194			
46	0.1562	.8262	1.4766	2.2984	2.9081	3.5133			
47	0.1564	.8245	1.4739	2.2944	2.9031	3.5073			
48	-0.1566	.8228	1.4712	2.2905	2.8983	3.5016			
49	- -0.1567	.8212	1.4687	2.2868	2.8937	3.4961			
50	0.1568	.8197	1.4663	2.2832	2.8892	3.4908			
51	-0.1570	.8182	1.4639	2.2797	2.8849	3.4856			
52	-0.1571	.8168	1.4616	2.2763	2.8807	3.4807			
53	— 0.1572	.8154	1.4594	2.2731	2.8767	3.4759			
54	— 0.1573	.8141	1.4573	2.2699	2.8728	3.4712			
	0.4555	0400	4 /550	0.000	0.000	2.400			
5 5	0.1575	.8128	1.4552	2.2669	2.8690	3.4667			
56	0.1576	.8116	1.4532	2.2639	2.8653	3.4623			
57	-0.1577	.8103	1.4512	2.2610	2.8618	3.4581			
58	-0.1578	.8092	1.4494	2.2583	2.8583	3.4540			
59	— 0.1579	.8080	1.4475	2.2556	2.8550	3.4500			
60	0.1580	.8069	1.4458	2.2529	2.8518	3.4461			
61	0.1580 0.1581	.8058	1.4456 1.4440	2.2529	2.8486	3.4424			
62	-0.1581 -0.1582	.8048	1.4424	2.2304	2.8455	3.4387			
63	-0.1582 -0.1583	.8038	1.4407	2.2475	2.8426	3.4352			
64	0.1583	.8028	1.4391	2.2433	2.8397	3.4317			
04	0.1303	.0020	1.4031	4.4404	2.0031	0.4317			

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TABLE 5.3 (continued)

Return period (years)

	Neturn perion (years)									
n	2	5	10	25	50	100				
65	0.1584	.8018	1.4376	2.2409	2.8368	3.4284				
66	-0.1585	.8009	1.4361	2.2387	2.8341	3.4251				
67	-0.1586	.8000	1.4346	2.2365	2.8314	3.4219				
68	-0.1587	.7991	1.4332	2.2344	2.8288	3.4188				
69	0.1587 0.1587	.7982	1.4318	2.2324	2.8263	3.4158				
03	-0.1367	.1302	1.4010	2.2021	2.0200	0.1200				
70	0.1588	.7974	1.4305	2.2304	2.8238	3.4128				
71	0.1589	.7965	1.4291	2.2284	2.8214	3.4099				
72	0.1590	.7957	1.4278	2.2265	2.8190	3.4071				
73	0.1590	.7950	1 4266	2.2246	2.8167	3.4044				
74	-0.1591	.7942	1.4254	2.2228	2.8144	3.4017				
75	0.1592	.7934	1.4242	2.2211	2.8122	3.3991				
76	0.1592	.7927	1.4230	2.2193	2.8101	3.3965				
77	0.1593	.7920	1.4218	2.2176	2.8080	3.3940				
78	— 0. 1593	.7913	1.4207	2.2160	2.8059	3.3916				
79	-0.1594	.7906	1.4196	2.2143	2.8039	3.3892				
80	0.1595	.7899	1.4185	2.2128	2.8020	3.3868				
81	0.1595	.7893	1.4175	2.2112	2.8000	3.3845				
82	0.1596	.7886	1.4165	2.2097	2.7982	3.3823				
83	0.1596	.7880	1.4154	2.2082	2.7963	3.3801				
84	0.1597	.7874	1.4145	2.2067	2.7945	3.3779				
85	0.1597	.7868	1.4135	2.2053	2.7927	3.3758				
86	0.1598	.7862	1.4125	2.2039	2.7910	3.3738				
87	-0.1598	.7856	1.4116	2.2026	2.7893	3.3717				
88	-0.1599	.7851	1.4107	2.2012	2.7877	3.3698				
89	0.1599	.7845	1.4098	2.1999	2.7860	3.3678				
90	0.1600	.7840	1.4089	2.1986	2.7844	3.3659				
91	0.1600	.7834	1.4081	2.1973	2.7828	3.3640				
92	-0.1601	.7829	1.4072	2.1961	2.7813	3.3622				
93	0.1601	.7824	1.4064	2.1949	2.7798	3.3604				
94	-0.1602	.7819	1.4056	2.1937	2.778 3	3.3586				
05	0.4000	7047	4 (0/0	2 4005	2.7769	3.3569				
95	0.1602	.7814	1.4048 1.4040	2.1925 2.1913	2.7754	3.3552				
96	0.1602	.7809				3.3532 3.3535				
97	0.1603	.7804	1.4033	2.1902	2.7740					
98	-0.1603	.7800	1.4025	2.1891	2.7726	3.3519				
99	0.1604	.7795	1.4018	2.1880	2.7713	3.3503				
100	-0.1604	.7791	1.4010	2.1869	2.7700	3.3487				
200	V.2001	•••								

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Extreme probability paper has a linear ordinate for the variable being studied, and the abscissa is a linear scale of the reduced variate [Eq. (5.3)]. For convenience in plotting, the warped scale of T_r is also shown along the top of Fig. 5.9. Plotting positions are commonly determined by the formulae [16]:

$$T_r = \frac{n+1}{m} \tag{5.4}$$

or

$$T_r = \frac{n + 0.4}{m - 0.3} \tag{5.5}$$

where n is the number of years of record (the number of items in the annual series) and m is the rank of the item on the series, m being 1 for the largest.

To illustrate the steps in numerical computation of the rainfall value for a given return period, hypothetical values of a series of annual rainfall maxima are given in the upper part of Table 5.4. Computations are illustrated in the lower part of the table for T_r of 10. Rainfall depths for return periods other than 10 years can be computed in a similar manner.

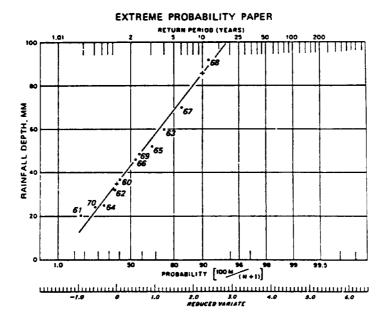


Figure 5.9 - Example of extreme probability plot using data of Table 5.4.

Table 5.4

Computation of extreme values

Year	P	m	$\frac{n+1}{m}$	$P - \overline{P}$	$(P - \overline{P})^2$	P ²
19 60	37	7	1.72	 9	81	1,369
1961	20	11	1.09	— 26	676	400
1962	32	8	1.5	14	196	1,024
1963	60	3	4.0	+ 14	196	3,600
1964	2 5	9	1.33	<u> </u>	441	625
1965	52	4	3.0	+6	36	2,704
1966	46	6	2.0	0	0	2,116
1967	70	2	6.0	+ 24	576	4,900
1968	92	1	12.0	+ 46	2,116	8,464
1969	48	5	2.4	+2	4	2,304
1970	24	10	1.2	 22	484	576
Total	506				4,806	28,082

$$\bar{P} = \hat{\Sigma} P/n = \frac{506}{11} = 46.0$$

$$s_x$$
 by square of deviations:
$$\sqrt{\frac{\sum_{n=1}^{\infty} (P)^2 - \overline{P} \sum_{n=1}^{\infty} P}{n-1}} = \sqrt{\frac{4806}{10}} = 21.92$$

s_x by short cut:
$$\sqrt{\frac{\sum\limits_{1}^{n}(P)^{2}-\overline{P}\sum\limits_{1}^{n}P}{n-1}}=\sqrt{\frac{4806}{10}}=21.92$$

For
$$T_r = 2$$
 and $n = 11$, $K = -0.1376$ (from Table 5.3).

Substituting into Eq. (5.1):

$$P_{\bullet} = 46.0 - 0.1376 \times 21.92 = 43.0$$

Similarly, for
$$T_r = 10$$
, $K = 1.8094$, and

$$P_{10} = 46.0 + 1.8094 \times 21.92 = 85.7$$

In Fig. 5.9 the two + 's show the above values for P_2 and P_{10} and define the line shown.

To illustrate the graphical method of fitting data to the extreme-value distribution, reference is again made to Table 5.4 and Fig. 5.9. In the table, values of the plotting position are given, and in Fig. 5.9 the plotted points are given, with rainfall values for each plotting position. The curve shown could have been drawn by fitting the plotted points by inspection.

In this example, for convenience, a record of only 11 years is used. Such a record gives a fairly stable value for return periods of as much as five years, but for longer return periods the short record has a large sampling error and the computations should not be taken as precise estimates.

For some types of data, instead of using the extreme-value distribution, a better fit of the data, or a closer approach to linearity, may be obtained from one of several other types of distribution, such as the normal or lognormal Pearson Type III distribution. A commonly used distribution is one in which the magnitude scale is logarithmic and the probability or return-period scale is the normal distribution. This distribution and the plotting paper used with it are widely known as log-normal. For discussion of additional distributions and of additional methods for fitting distributions, reference may be made to textbooks, and periodical statistical literature [17, 18, 63-66].

An advantage of fitting data to a distribution is achievement of objectivity. This advantage has the corollary of standard treatment of data, so that a decision is based on differences in data rather than differences in subjective interpretation of data. A third advantage of linearity in plotting points, and of close fit to a particular distribution, is the facility for extrapolating beyond the range of the data. However, it should be remembered that extrapolation involves considerable sampling error.

For evaluation of the accuracy of the computed values X_{T_r} it would be desirable to compute the confidence interval with limits:

$$X_{T_r}$$
— $t(\alpha) s_e$; $X_{T_r} + t(\alpha) s_e$

within which, with given confidence levels, one may expect to find the true precipitation value X_{T_r} . Values of $t(\alpha)$ for selected confidence levels are as follows:

$\alpha = 95 \%$	$t(\alpha) = 1.960$
$\alpha = 90 \%$	$t(\alpha) = 1.645$
$\alpha = 80 \%$	$t(\alpha) = 1.282$
$\alpha = 68 \%$	$t(\alpha) = 1.000$

In most cases, values of se, the standard error of estimate, can be computed by means of the formula

$$s_e = \beta_{T_p} \cdot \frac{s_x}{\sqrt{n}} \tag{5.6}$$

In particular, for the Gumbel distribution the following relation [19] exists:

$$\beta_{\rm T_r} = \sqrt{1 + 1.14 \, \text{K} + 1.10 \, \text{K}^2} \tag{5.7}$$

where K is the numerical value defined by Eq. (5.2) and readily obtainable from Table 5.3. However, for convenience in the use of Eq. (5.6) values of β_{T_r}/\sqrt{n} can be obtained directly from Table 5.5. Thus, in determining the 80 per cent confidence interval for $P_{10} = 85.7$ in Table 5.4, for example,

$$t(a)s_e = 1.282 \times 0.7783 \times 21.92 = 21.9$$

The lower and upper limits of the confidence interval are therefore 85.7-21.9 and 85.7+21.9, respectively, which means that there is an 80 per cent probability that the true value of P_{10} lies between 63.8 and 107.6. Similarly, the lower and upper limits of the same confidence interval for $P_2=43.0$ are 35.1 and 50.9, respectively, the value of β_{T_r}/\sqrt{n} being 0.2803 (Table 5.5).

Table 5.5

Values of β_{T_r}/\sqrt{n} for use in Eq. (5.6)

Return period (years)

Return period (years)								
n	2	5	10	25	50	100		
10	.2942	.5863	.8285	1.1472	1.3873	1.6273		
11	.2803	.5522	.7783	1.0761	1.3007	1.5252		
12	.2681	.5232	.7358	1.0161	1.2275	1.4389		
13	.2574	.4982	.6992	.9645	1.1646	1.3648		
14	.2479	.4763	.6673	.9196	1.1100	1.3005		
15	.2393	.4569	.6392	.8801	1.0620	1.2439		
16	.2316	.4397	.6142	.8450	1.0193	1.1937		
17	.2246	.4242	.5918	.8136	.9811	1.1488		
18	.2182	.4102	.5716	.7853	.9467	1.1083		
19	.2123	.3974	.5532	.7596	.9155	1.0716		
20	.2068	.3857	.5365	.7361	.8871	1.0382		
21	.2018	.3750	.5211	.7146	.8610	1.0075		
22	.1971	.3651	.5069	.6948	.8370	.9793		
23	.1927	.3559	.4937	.6765	.8148	.9532		
24	.1886	.3473	.4815	.6595	.7942	.9290		
25	.1847	.3394	.4702	.6437	.7750	.9064		
26	.1811	.3319	.4595	.6289	.7571	.8854		
27	.1777	.3249	.4496	.6150	.7403	.8657		
28	.1745	.3183	.4402	.6020	.7245	.8472		
29	.1714	.3121	.4314	.5898	.7097	.8298		
30	.1685	.3062	.4230	.5782	.6957	.8134		
31	.1657	.3007	.4152	.5673	.6825	.7978		
32	.1631	.2954	.4077	.5569	.6699	.7831		
33	.1606	.2904	.4006	.5471	.6581	.7692		
34	.1582	.2856	.3938	.5377	.6468	.7559		
35	.1559	.2811	.3874	.5289	.6360	.7433		
36	.1537	.2767	.3813	.5204	.6257	.7313		
37	.1516	.2726	.3754	.5123	.6159	.7198		
38	.1496	.2686	.3698	.5045	.6066	.7088		
39	.1476	.2648	.3645	.4971	.5976	.6983		

(continued)

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TABLE 5.5 (continued)

Return period (years)

		Reli	urn period (y	iears j		
n	2	5	10	25	50	100
40	.1457	.2611	.3593	.4900	.5890	.6883
41	.1439	.2576	.3544	.4832	.5808	.6786
42	.1422	.2542	.3496	.4766	.5729	.6693
43	.1405	.2510	.3451	.4703	.5653	.6604
44	.1389	.2479	.3407	.4643	.5580	.6518
45	.1373	.2449	.3365	.4584	.5509	.6 43 6
45 46	.1373	.2419	.3324	.4528	.5441	.6356
47	.1344	.2391	.3284	.4326	.5375	.6279
47	.1344	.2364	.3246	.4474	.5312	.6205
					.5251	
49	.1316	.2338	.3209	.4370	.5251	.6133
50	.1303	.2312	.3174	.4321	.5192	.6064
51	.1290	.2288	.3139	.4274	.5134	.5996
52	.1277	.2264	.3106	.4228	.5079	.5931
53	.1265	.2241	.3073	.4183	.5025	.5868
54	.1253	.2218	.3042	.4140	.4973	.5807
55	.1242	.2196	.3012	.4098	.4922	.5748
5 6	.1230	.2175	.2982	.4057	.4873	.5690
57	.1219	.2155	.2953	.4018	.4825	.5635
58	.1209	.2135	.2925	.3979	.4779	.5580
59	.1198	.2115	.2898	.3942	.4734	.5527
60	.1188	.2096	.2872	.3905	.4690	.5476
61	.1179	.2078	.2846	.3870	.4647	.5426
62	.1179	.2078	.2821	.3836	.4647	.5377
63	.1160	.2042	.2796	.3802	.4565	.5330
64	.1150	.2025	.2772	.3769	.4525	.5284
65	.1142	.2008	.2749	.3737	.4487	.5239
66	.1133	.1992	.2726	.3706	.4449	.5195
67	.1124	.1976	.2704	.3676	.4413	.5152
68	.1116	.1960	.2683	.3646	.4377	.5110
69	.1108	.1945	.2661	.3617	.4342	.5069
70	.1100	.1930	.2641	.3589	.4208	.5029
71	.1092	.1916	.2621	.3561	.4274	.4990
$\frac{72}{72}$.1084	.1902	.2601	.3534	.4242	.4952
73	.1077	.1888	.2582	.3507	.4210	.4914
74	.1070	.1874	.2563	.3481	.4179	.4878
		12017	.=000	.0401	.4110	. 4010

		HYDR	OLOGICAL AN	ALYSIS		5.29
		Тав	LE 5.5 (cont	inued)		
		Ret	urn period (y	ears)		
n	2	5	i o	25	50	100
75	.4062	.1861	.2544	.3456	.4148	.4842
76	.1055	.1848	.2526	.3431	.4118	.4807
77	.1048	.1835	.2508	.3407	.4089	.4773
78	.1042	.1823	.2491	.3383	.4060	.4739
79	.1035	.1810	.2474	.3360	.4032	.4706
80	.1028	.1798	.2457	.3337	.4005	.4674
81	.1022	.1786	.2441	.3315	.3978	.4643
82	.1016	.1775	.2425	.3293	.3951	.4612
83	.1010	.1764	.2409	.3271	.3925	.4581
84	.1004	.1752	.2394	.3250	.3900	.4552
85	.0998	.1742	.2379	.3229	.3875	.4522
86	.0992	.1731	.2364	.3209	.3850	.4494
87	.0986	.1720	.2349	.3189	.3826	.4466
88	.0980	.1710	.2335	.3169	. 38 03	.4438
89	.0975	.1700	.2321	.3150	.3780	.4411
90	.0969	.1690	.2307	.3131	.3757	.4384
91	.0964	.1680	.2293	.3113	.3734	.4358
92	.0959	.1670	.2280	.3094	.3712	.4332
93	.0954	.1661	.2267	.3076	.3691	.4307
94	.0948	.1652	.2254	.3059	.3670	.4282
95	.0943	.1642	.2241	.3041	.3649	.4258
96	.0939	.1633	.2229	.3024	.3628	.4234
97	.0934	.1624	.2217	.3007	.3608	.4210
98	.0929	.1616	.2204	.2991	.3588	.4187
99	.0924	.1607	.2193	.2975	.3569	.4164
100	.0919	.1599	.2181	.2959	.3549	.4142

An example of the magnitude of error in extrapolation beyond the range of the data may be found in the record of maximum annual 24-hour rainfall at Hartford, Connecticut, U.S.A. Based on the 50 years of record through 1954, the 100-year value was found to be 155 mm. The maximum event during this period was 170 mm. In 1955 a hurricane produced 307 mm in 24 hours. The computation of 100-year 24-hour rainfall based on the 51 years of record through 1955 resulted in a new estimate of 218 mm, a 40 per cent increase. Even the 10-year value was increased substantially by this one event.

5.30 HYDROLOGICAL ANALYSIS

It may happen, however, that during a definite period of T_r years, precipitation of the magnitude $P \ge P_{T_r}$ does not occur at all, or that it occurs several times. The probability that, during a given period of t years, a respective phenomenon will occur n times, is equal to

$$Pr_{n/t} = \left(\frac{t!}{n!(t-n)!}\right) p^{n} (1-p)^{t-n}$$
 (5.8)

where $p=1/T_r$. Assuming, for example, that $t=T_r=100$ years, then the probabilities for various values of n are:

n	0	1	2	3	4	5
$Pr_{n/100}$	0.366	0.370	0.185	0.061	0.015	0.003

The overall probability of $P_{\mathrm{T_r}}$ or greater event occurring in t years is discussed in Sec. A.5.7.3.